## INFLUENCE OF THE LIGATION METHOD, METALLIC ALLOY AND TIPPING IN SLIDING MECHANICS João Cavaleiro, Luísa Maló, Francisco Vale

## OBJECTIVES

To evaluate, in vitro:
a. the resistance to sliding of conventional ligated brackets and self-ligating brackets when using stainless steel and nickel-titanium archwires
b. the effect of tipping on the resistance to sliding mechanics.

## MATERIALS and METHODS

The 0.022 -inch slot brackets Damon ${ }^{\circledR} \mathrm{Q}^{\text {TM }}$, Prodigy $\mathrm{SL}^{\text {™ }}$ (Sybron Dental Specialties Ormco ${ }^{\text {TM }}$, Orange, Califórnia, USA), Smart-Clip ${ }^{\text {TM }}$ SL3, Victory Series ${ }^{\text {™ }}$ (3M Unitek Orthodontic Products, Monrovia, Califórnia, USA), Morelli® Roth Standard and Morelli® ${ }^{\circledR}$ Roth SLI (Morelli Ortodontia, Sorocaba, São Paulo, Brazil) were tested. The brackets were ligated to $0.016 \times 0.022$ inch stainless steel (Dentaurum GmbH, Ispringen, Germany) and nickel-titanium (DM Ceosa, Madrid, Spain) archwires. A tipping of 00 or 50 was added to the wires. For each combination of bracket/ archwire, 10 sliding tests were performed with the Shimadzu AG-1 5kN testing instrument (Shimadzu Corporation, Tokyo, Japan) (Figure 2). Maximum registered resistance to sliding was measured throughout 5 mm translation of the archwire, at a crosshead speed of $10 \mathrm{~mm} / \mathrm{min}$.

## RESULTS

Table 1 - Resistance to sliding registered for each type of bracket, according to archwire alloy and tipping.

* Elastomeric ligation

| Archwire Alloy | Tipping | Conventional Brackets |  |  | Passive Self-ligating Brackets |  |  | Active Self-ligating Brackets |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Mean ( $\sigma$ ) | Minimum | Maximum | Mean ( $\sigma$ ) | Minimum | Maximum | Mean ( $\sigma$ ) | Minimum | Maximum |
|  | 0 degrees | 3.85 (1.46) | 2.19 | 6.00 | 0.10 (0.02) | 0.08 | 0.14 | 0.11 (0.03) | 0.07 | 0.17 |
| Stainless Steel | 0 degrees* |  |  |  | 2.42 (0.31) | 2.08 | 2.76 | 3.05 (0.59) | 1.99 | 3.98 |
|  | 5 degrees | 3.20 (1.01) | 1.71 | 5.15 | 0.47 (0.39) | 0.08 | 1.23 | 0.18 (0.05) | 0.10 | 0.24 |
|  | 0 degrees | 4.24 (0.87) | 2.83 | 5.28 | 0.11 (0.02) | 0.08 | 0.15 | 0.13 (0.05) | 0.08 | 0.26 |
| NickelTitanium |  |  |  |  |  |  |  |  |  |  |
|  | 5 degrees | 3.38 (0.90) | 2.03 | 4.70 | 0.14 (0.03) | 0.10 | 0.20 | 0.11 (0.02) | 0.07 | 0.15 |



Figure 1 - Resistance to sliding test graphic obtained by Shimadzu AG-1 5kN testing instrument.


Figure 2 - Shimadzu AG-1 5kN testing instrument.

- Conventional brackets show higher resistance to sliding when comparing to active or passive self-ligating brackets ( $p<0,001$ ) (Kruskal-Wallis and Mann-Whitney post-hoc tests).
- No statistically significant differences were found between the resistance to sliding of active and passive self-ligating brackets (student t-test for independent samples).
- No statistically significant differences were found between archwire alloys at 0 degrees angulation (Non-parametric Mann-Whitney test for independent samples).
- For 5 degrees angulation stainless steel archwires show statistically significant higher resistance to sliding ( $\mathrm{p}=0,004$ ) (Non-parametric Mann-Whitney test for independent samples).
- No statistically significant differences were observed between 0 and 5o of tipping (student t-test for independent samples).


## CONCLUSIONS

Self-ligating brackets are an useful tool in orthodontic mechanics when low friction levels are needed. If coupled with small diameter archwires, the resistance to sliding is not affected by small angulations and low degrees of tipping. Nevertheless, different metallic alloys present dissimilar behavior when tipping angulations are present.

